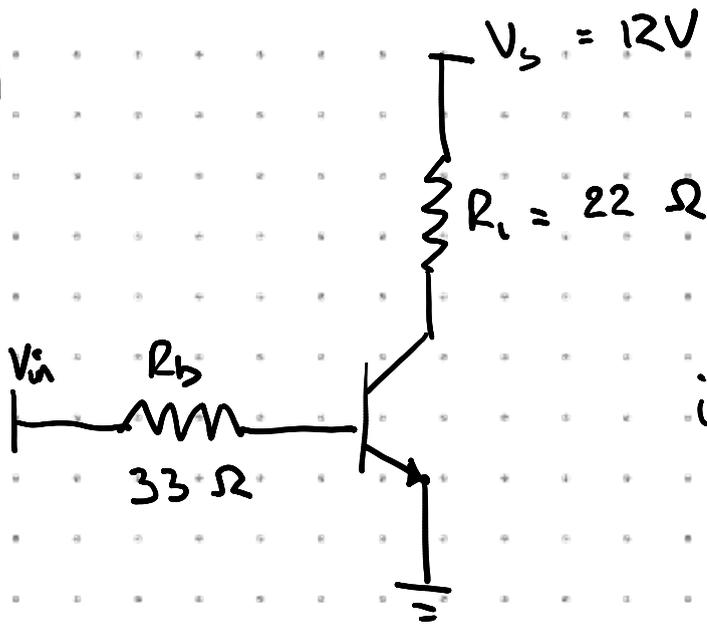


Chapter 1: Transistors

1.1



$$\beta = 25$$

$$V_{ce(sat)} = 0,2V$$

$$V_{in} = 3,3V$$

$$i_c = i_c = \frac{12 - 0,2}{22}$$

$$= 0,536 A$$

$$i_b = \frac{3,3 - 0,7}{33}$$

$$= 0,0788 A$$

Max current that can be supplied by $\beta = 25$:

$$i_{c(max)} = \beta \cdot i_b$$

$$= 25 \cdot 0,0788$$

$$= 1,97 A \quad (>> 0,536 A \therefore \text{saturated})$$

$$\beta_{eff} = \frac{i_c}{i_b} = \frac{0,536}{0,0788}$$

$$= 6,80 \rightarrow$$

The load limits i_c here

1.2 Same circuit but $R_L = 5\Omega$

$$i_c = \frac{12 - 0,2}{5} = 2,36 \text{ A} \quad (i_c \text{ saturated})$$

$$i_b = 0,0788$$

Max current that can be supplied by $\beta = 25$:

$$i_{c(\max)} = 1,97 \text{ A}$$

As $2,36 \text{ A} > 1,97 \text{ A}$ Transistor cannot reach saturation

$$\therefore \beta_{eff} = 25$$

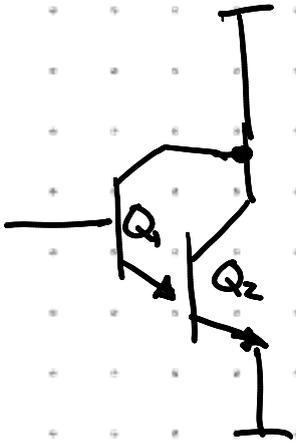
$$\text{and } i_c = 1,97 \text{ A}$$

(limited by the transistor β)
& i_b

$$\begin{aligned} \therefore V_c &= i_c \cdot R_c \\ &= 1,97 \cdot 5 \\ &= 9,85 \text{ V} \end{aligned}$$

$$\begin{aligned} \text{and } \therefore V_{ce} &= 12 - 9,85 \\ &= \underline{\underline{2,15 \text{ V}}} \end{aligned}$$

1.3



$$i_c = \beta i_b$$

$$i_e = i_b + i_c$$

$$\begin{aligned} i_{c1} &= i_{b1} + \beta_1 i_{b1} \\ &= (\beta_1 + 1) i_{b1} = i_{b2} \end{aligned}$$

$$i_{c_{total}} = i_{c1} + i_{c2}$$

$$i_{c1} = \beta_1 i_{b1}$$

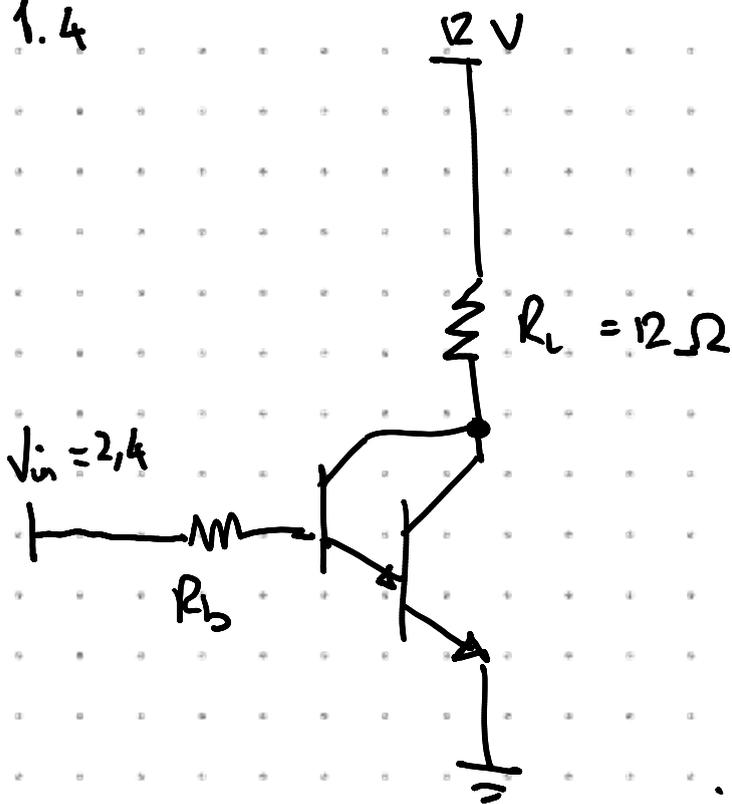
$$i_{c2} = \beta_2 i_{b2} = \beta_2 (\beta_1 + 1) i_{b1}$$

$$\begin{aligned} \therefore i_{c_{total}} &= \beta_1 i_{b1} + \beta_2 (\beta_1 + 1) i_{b1} \\ &= (\beta_1 + \beta_2 \beta_1 + \beta_2) i_{b1} \end{aligned}$$

$$\begin{aligned} \beta_{total} &= \frac{i_{c_{total}}}{i_{b1}} = \beta_1 + \beta_2 \beta_1 + \beta_2 \\ &= \beta_1 (\beta_2 + 1) + \beta_2 \end{aligned}$$

$$\text{As } \beta_2 \gg 1 \quad \beta_{total} \rightarrow \beta_2 \beta_1$$

1.4



$$\beta > 1000$$

for saturation, $V_{CE\text{sat}} = 0,2V$

$$\begin{aligned} \therefore i_{c(\text{sat})} &= \frac{12 - 0,2}{12} \\ &= 0,983 \text{ A} \end{aligned}$$

$$\begin{aligned} i_b &> \frac{i_c}{\beta_{\text{min}}} \\ &> \frac{0,983}{1000} \\ &> 0,983 \text{ mA} \end{aligned}$$

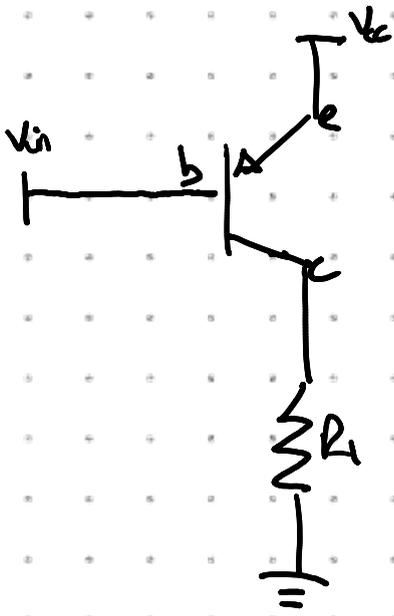
$$i_b > \frac{V_{in} - 1,4}{R_b}$$

$$R_b < \frac{2,4 - 1,4}{0,000983}$$

$$R_b < 1017 \Omega$$

\therefore choose $R_b = 560\Omega$ (E12) \rightarrow

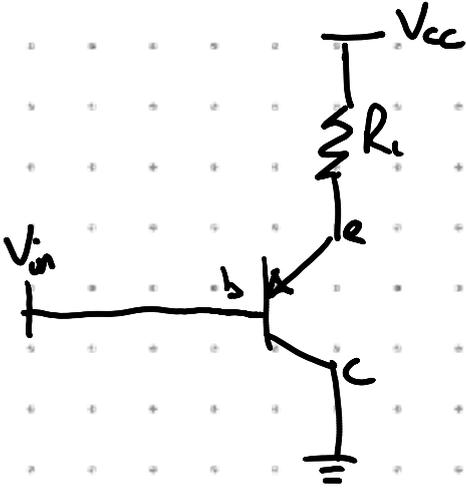
1.5



Ground connected load without R_B

When $V_{in} = 0V$ there is a short from V_{cc} to GND through the b-e junction.

→ Need R_B to prevent short.

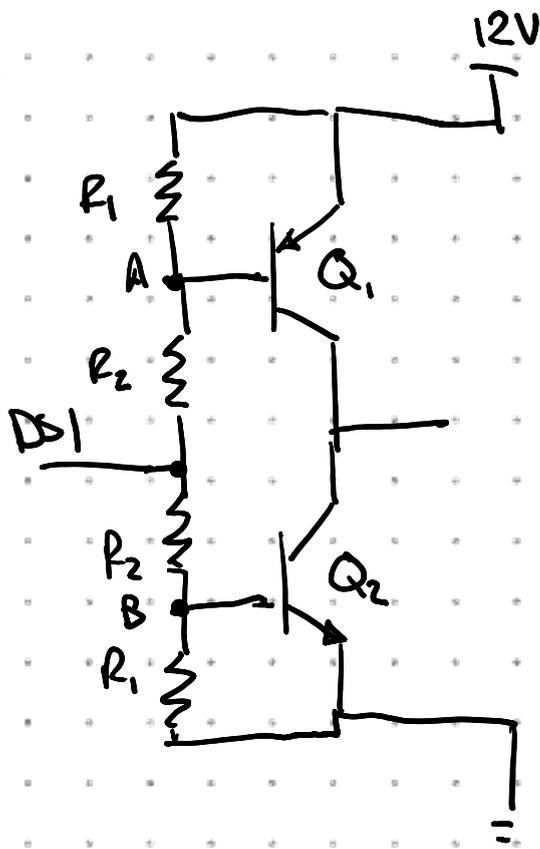


Supply connected load without R_B
is fine as when $V_{in} = 0V$,

R_L itself limits the current through b-e, preventing the short

1.6 Without the resistors to the bases, when D_{S1} or D_{S2} is low (V_- or GND) the top transistors would short circuit through b_e , when D_{S1} or D_{S2} is high (V_+) the bottom transistors would short through $b-e$.

1.7



$$\beta = 1000$$

$$R_1 = 180 \Omega$$

$$R_2 = 1 \text{ k}\Omega$$

When $DS1 = 12 \text{ V}$:

$$V_A = 12 \text{ V} \quad \therefore Q_1 \text{ OFF}$$

$$V_B = 12 \cdot \frac{R_1}{R_1 + R_2}$$

$$= 12 \cdot \frac{180}{1180} = 1,83 \text{ V}$$

$$\therefore Q_2 \text{ ON}$$

When $DS1 = 0 \text{ V}$:

$$V_A = 12 \cdot \frac{1000}{1180}$$

$$= 10,17 \text{ V} \quad \therefore Q_1 \text{ ON}$$

$$V_B = 0 \text{ V} \quad \therefore Q_2 \text{ OFF}$$

When $V_{SI} = 6 \text{ V}$:

$$V_B = 6 \cdot \frac{180}{1180}$$

$$= 0,915 \text{ V} \quad \therefore Q_2 \text{ OFF}$$

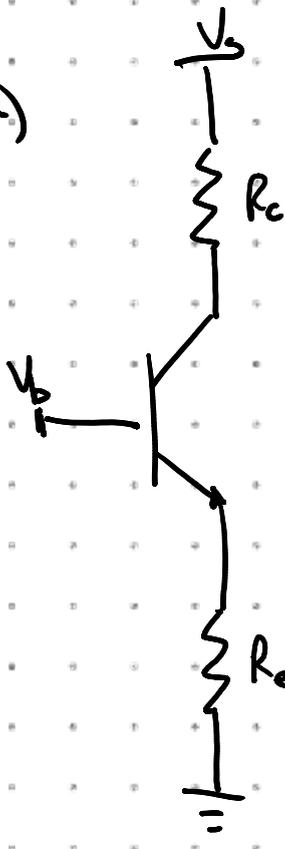
$$V_A = 6 + (12-6) \cdot \frac{1000}{1180}$$

$$= 11,08 \text{ V}$$

$\therefore Q_1 \text{ OFF}$

1,8

a)



$$V_e = V_b - 0,7$$

$$i_e = \frac{V_e}{R_e} = \frac{V_b - 0,7}{R_e}$$

$$i_c = \left(\frac{\beta}{\beta+1} \right) i_e$$

$$\therefore i_c = \left(\frac{\beta}{\beta+1} \right) \left(\frac{V_b - 0,7}{R_e} \right)$$

$$\text{and } i_c = \frac{V_s - V_c}{R_c}$$

$$\therefore V_s - V_c = R_c \left(\frac{\beta}{\beta+1} \right) \left(\frac{V_b - 0,7}{R_e} \right)$$

$$\therefore \frac{V_s - V_c}{V_b - 0,7} = \frac{R_c}{R_e} \cdot \frac{\beta}{\beta+1}$$

